

# Design Criteria for the HTR Core

Jan Leen Kloosterman, Physics of Nuclear Reactors, TU-Delft  
20-11-2008

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Safety

The diagram consists of two overlapping circles. The top circle is green and labeled 'Safety'. The bottom circle is red and labeled 'Economy'. The overlapping area in the center is shaded in a darker red. A small black dot is located within this overlapping area.

Economy

# What is Nuclear Safety?

Target: no health hazard to the public or personnel

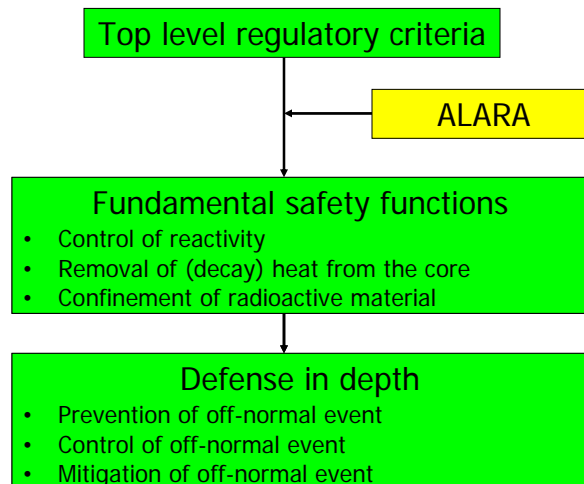
Subtargets:

- ⚠ No one near the boundary should take shelter or be evacuated
- ⚠ No need for moving mechanical components to ensure this target
- ⚠ Exposure to plant personnel significantly lower than current international values



Koster *et al.*, Nucl. Eng. Des. 222(2003) 231

# Safety design philosophy



# Safety classification in defense of depth

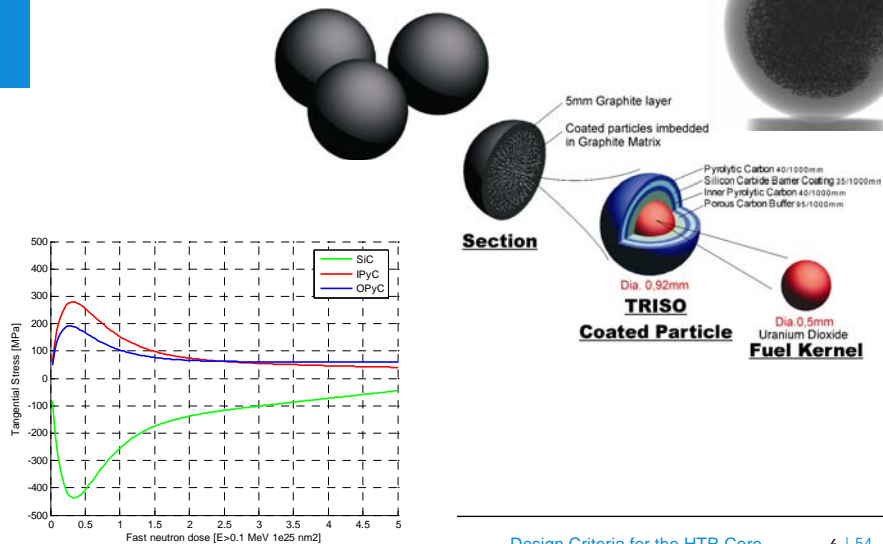
## Prevention systems

1. Systems that can cause damage to the core if not working properly (inwp)
2. Systems that can cause fission product release inwp
3. Systems that can trigger off-normal events inwp

## Mitigation systems

1. Systems to stop the reactor rapidly and remove residual heat
2. Systems to reduce radiation exposure to the public
3. Countermeasures and systems in off-normal states

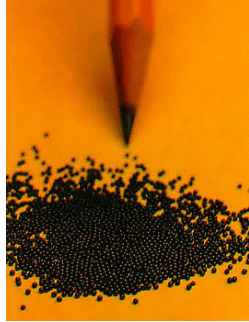
# Fission product containment



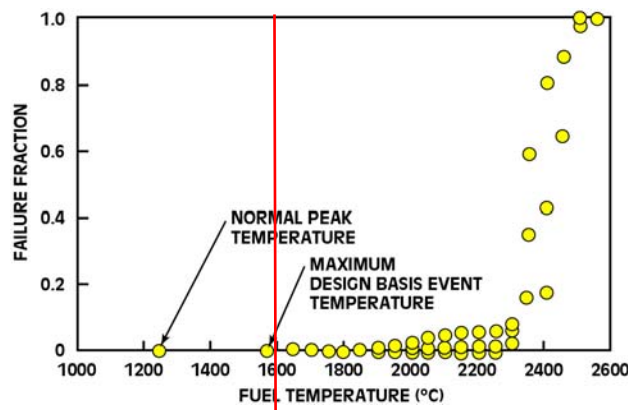
# Fission product containment

HTR

LWR



# Fission product containment



Considered to be a safe lower temperature limit

## Decay heat production

### 1) Fission products decay

$\beta^-$  production ( $\approx 8$  MeV/fission),  $\gamma$ -rays ( $\approx 7$  MeV/fission)

### 2) Actinide decay

U-239 (23.5 min) and Np-239 (2.35 days)

Much more important for irradiated MOX fuel

### 3) Delayed neutron induced fission

Comparable to fission products decay; time span?

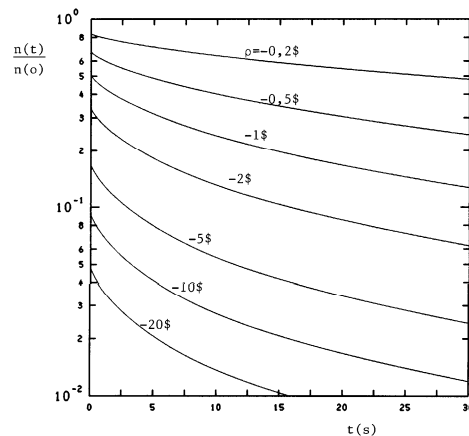
### 4) Spontaneous fission

Much more a shielding problem than decay heat

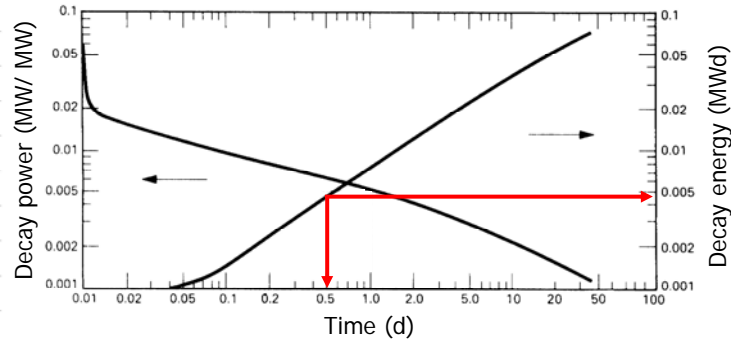
### 5) Activation of structural materials (only few % of FP decay heat)

## Decay heat production

$$P(t) \approx P_0 \left[ \left( \frac{\beta}{\beta - \rho_0} \right) \exp(-\lambda t) - \left( \frac{\rho_0}{\beta - \rho_0} \right) \exp\left( \frac{\rho_0 - \beta}{\Lambda} t \right) \right]$$



## Decay heat production



Source: ORNL

## Decay heat production

Produced heat after 0.5 day amounts:

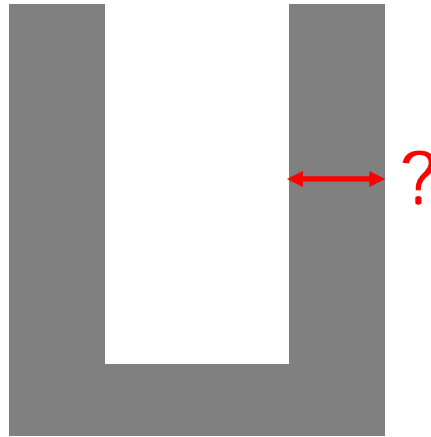
$$0.0047 \text{ MWd} \approx 400 \text{ MWs} = 400 \text{ fps}$$

Heat reservoir in BWR	Energy (fps)
Fuel from operating temp to $100^{\circ}\text{C}$	9
Coolant from $286^{\circ}\text{C}$ to $100^{\circ}\text{C}$	112
Reactor vessel and internals	43

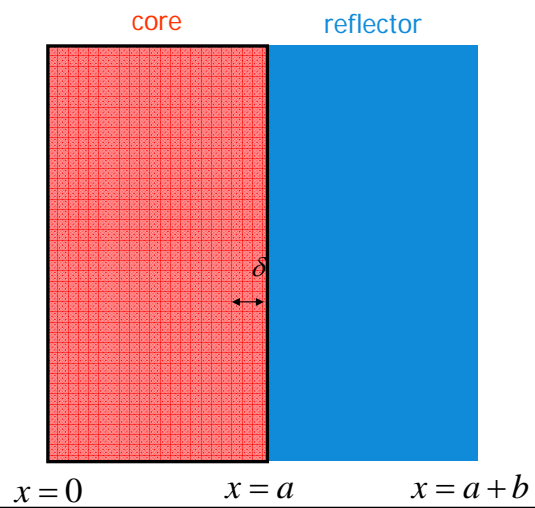
(Pershagen, Light Water Reactor Safety, 1989)  
(J.L.Kloosterman, FJOH summerschool, 2000)



## Pebble-bed reactor core design



## Reflector savings

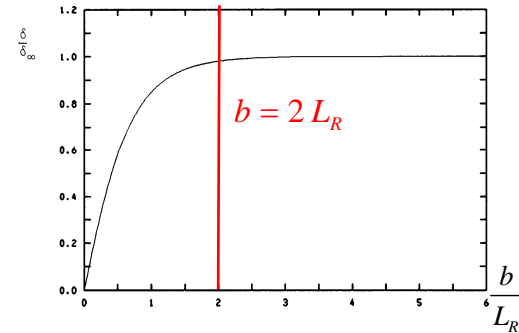


## Reflector savings

$$\delta = a(\text{bare}) - a(\text{refl}) = \frac{1}{B_{mC}} \tan^{-1} \left( \frac{D_C B_{mC}}{D_R} L_R \tanh \frac{b}{L_R} \right)$$

Thick reflector ( $b \gg L_R$ )

$$\delta \rightarrow \delta_\infty = \frac{D_C}{D_R} L_R$$



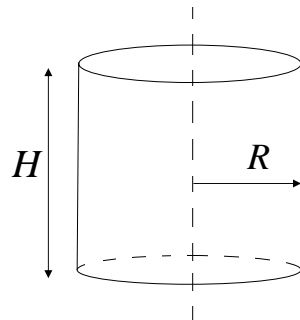
## Reflector savings

TABLE 8-7: Diffusion Parameters for Some Common Moderators

Moderator	Density (g/cm <sup>3</sup> )	D(cm)	$\Sigma_a(\text{cm}^{-1})$	$L(\text{cm})$	$\tau_{th}(\text{cm}^2)$	$M(\text{cm})$
H <sub>2</sub> O	1.00	0.16	0.0197	2.85	26	5.84
D <sub>2</sub> O	1.10	0.87	$2.9 \times 10^{-5}$	170	131	170
Be	1.85	0.50	$1.0 \times 10^{-3}$	21	102	23
Graphite	1.60	0.84	$2.4 \times 10^{-4}$	59	368	62

Duderstadt and Hamilton, Nuclear Reactor Analysis, 1976

## Low leakage core design



$$P_{NL} = P_{FNL} \cdot P_{TNL}$$

$$= \frac{1}{1 + B_g^2 \tau} \cdot \frac{1}{1 + B_g^2 L^2}$$

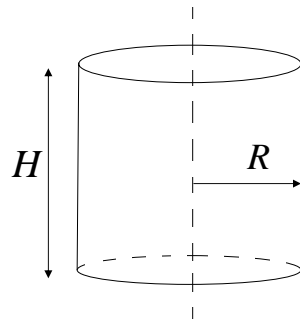
$$\approx \frac{1}{1 + B_g^2 M^2}$$

$\tau$  is a measure for the rms distance travelled until the neutron reaches the thermal energy range

$L^2$  is a measure for the rms distance a thermal neutron travels until it is absorbed

$M^2$  is migration area

## Low leakage core design



$$H = 1.85 R$$

$$\nabla^2 \phi + B_g^2 \phi = 0$$

$$\frac{1}{r} \frac{\partial}{\partial r} r \frac{\partial \phi}{\partial r} + \frac{\partial^2 \phi}{\partial z^2} + B_g^2 \phi = 0$$

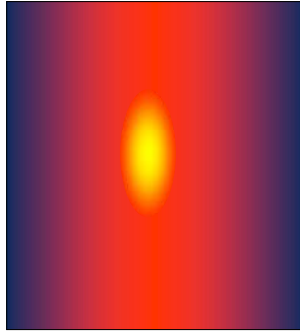
$$\phi(r, z) = \mathfrak{R}(r) \cdot Z(z)$$

$$\phi(r, z) = A J_0 \left( \frac{v_0 r}{\tilde{R}} \right) \cos \left( \frac{\pi z}{\tilde{H}} \right)$$

$$B_g^2 = \left( \frac{v_0}{\tilde{R}} \right)^2 + \left( \frac{\pi}{\tilde{H}} \right)^2$$

## Reactor core design

DLOFC

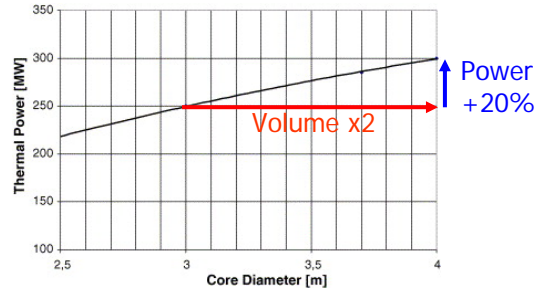
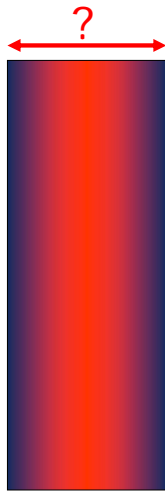


Passive decay  
heat removal  
calls for long tall  
reactor cores

## Reactor core design



## Reactor core design

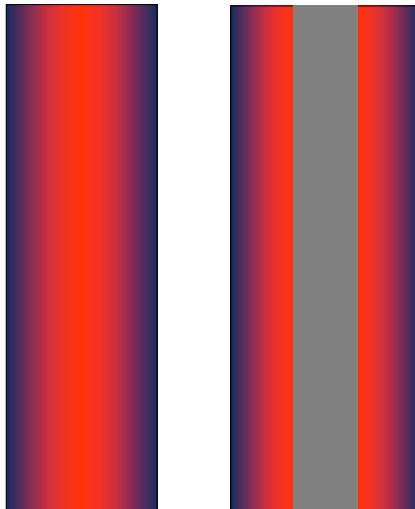


Ben Said et al, Nucl Eng Des, 236(2006) 648

Core diameter limited by

- shutdown capability
- RPV diameter
- decay heat removal

## Reactor core design



Passive decay heat removal calls for long tall reactor cores

*Or*

Cores with a fuel-free central column

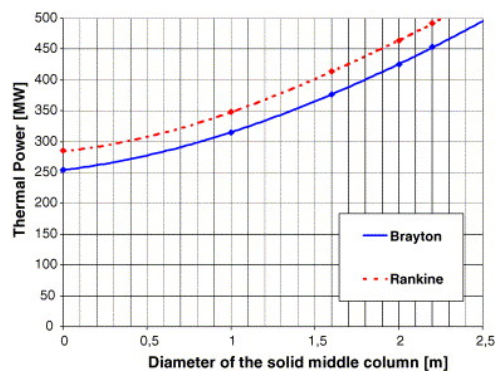
## Reactor core design



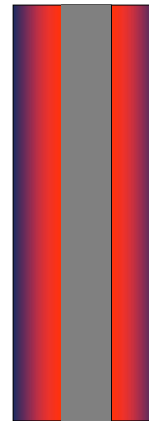
<i>Design</i>					
Core height [m]	11			11	
Inner core diameter [m]	-			2	
Outer core diameter [m]	3			3.7	
RPV outer diameter [m]	5.7			6.4	
<i>Variant</i>	<i>Brayton</i>	<i>Rankine</i>	<i>Brayton</i>	<i>Rankine</i>	
Inlet temperature [°C]	500	250	500	250	
Outlet temperature [°C]	900	750	900	750	
<b>Thermal power [MW]</b>	<b>220</b>	<b>250</b>	<b>425</b>	<b>464</b>	
Mean power density [MW/m <sup>3</sup> ]	2.83	3.21	5.07	5.54	
Helium mass flow rate [Kg/s]	105.9	96.24	204.5	178.6	
Pressure drop over the core [bar]	1.27	0.84	3.55	2.18	

Ben Said et al, Nucl Eng Des, 236(2006) 648

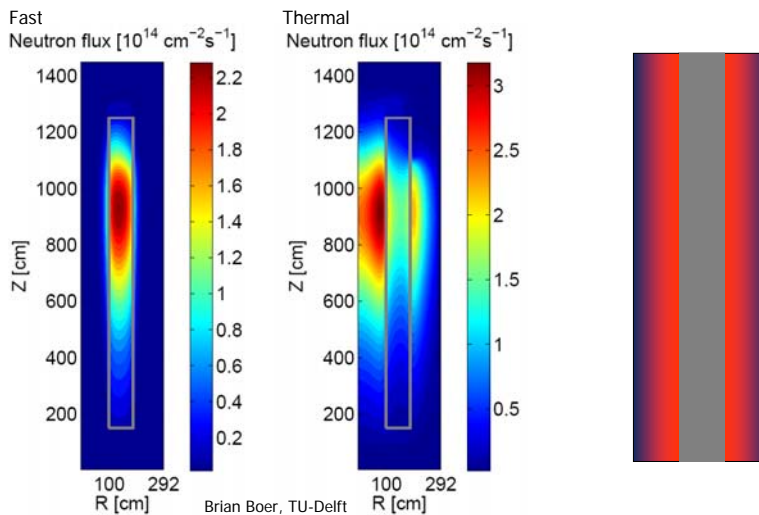
## Reactor core design



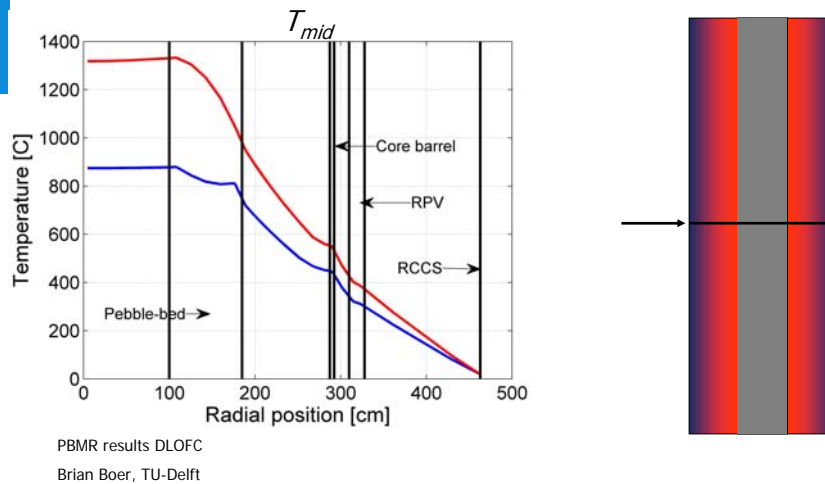
Ben Said et al, Nucl Eng Des, 236(2006) 648



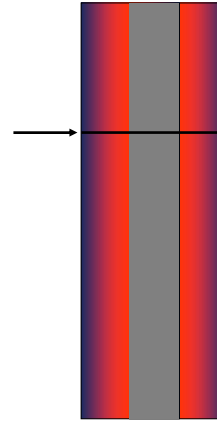
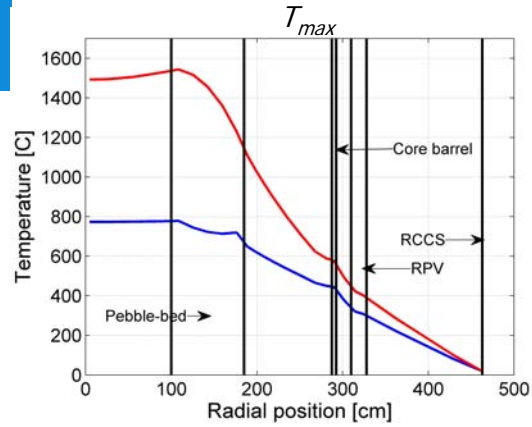
## Neutron flux profile



## Reactor core design

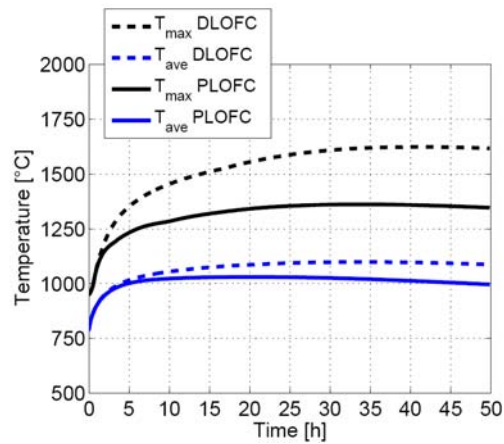


## Reactor core design



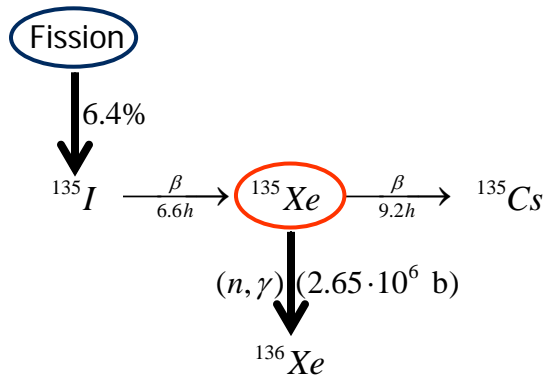
PBMR results DLOFC  
Brian Boer, TU-Delft

## Pressurized and Depressurized LOFC

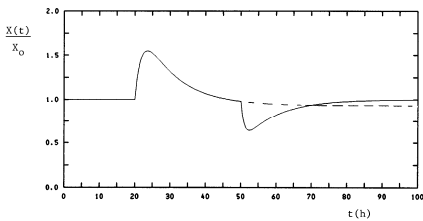
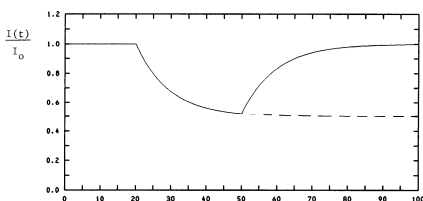
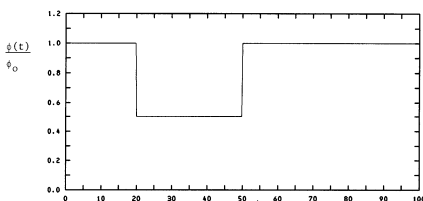


Brian Boer, TU-Delft

## Maximum core height



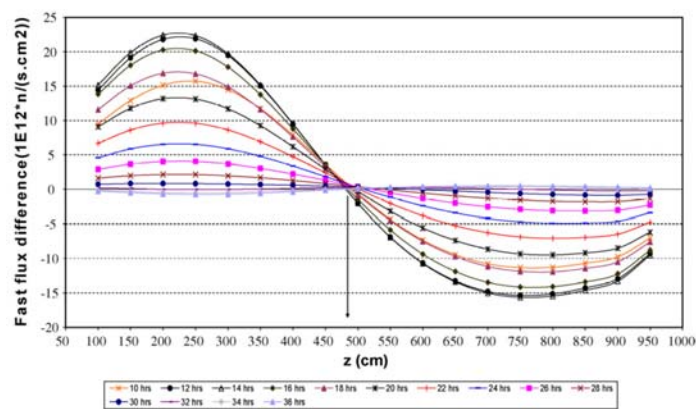
$\Phi \uparrow \Rightarrow [\text{Xe}] \downarrow \Rightarrow \rho \uparrow \Rightarrow \Phi \uparrow$  Positive feedback !



## Xenon oscillations

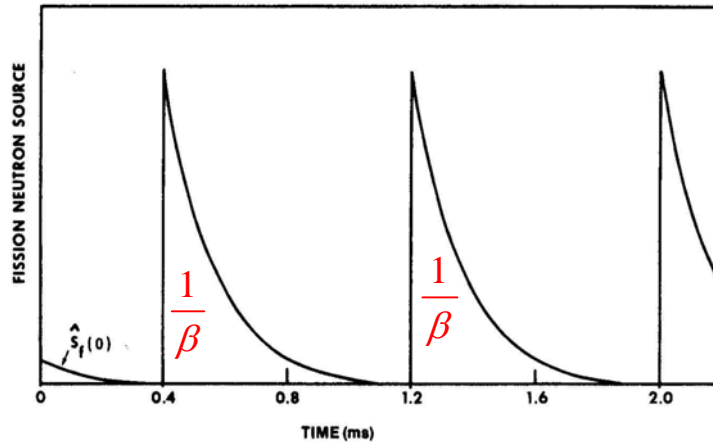


## Xenon oscillations



Strydom, Nucl Eng Des, 238(2008) 2960

## Maximum core height



Ott and Neuhold, Introductory Dynamics of Nuclear Reactors

## Maximum core height

Migration area: 
$$M^2 = L^2 + \tau = \frac{1}{6} \langle \ell^2 \rangle$$

( $L$  diffusion length,  $\tau$  Fermi age)

Squared prompt fission chain length: 
$$L_{PFC}^2 = \frac{1}{\beta} \langle \ell^2 \rangle = \frac{1}{\beta} 6M^2$$

Prompt fission chain length: 
$$L_{PFC} = \sqrt{\frac{6}{\beta} \langle \ell^2 \rangle} \approx 30M$$

Any core larger than  $30M$  is loosely coupled  
and therefore sensitive to Xenon oscillations

# Maximum reactor core height

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Reactor Type	$\langle L \rangle$ (cm)	$\tau_{th}$ (cm <sup>2</sup> )	$\langle M \rangle$ (cm)	Diameter	
				$\langle M \rangle$	$\langle L \rangle$
PWR	1.8	40	6.6	56	190
BWR	2.2	50	7.3	50	180
HTGR	12.0	300	21	40	63
LMFBR	5.0	-	-	-	35
GCFR	6.6	-	-	-	35

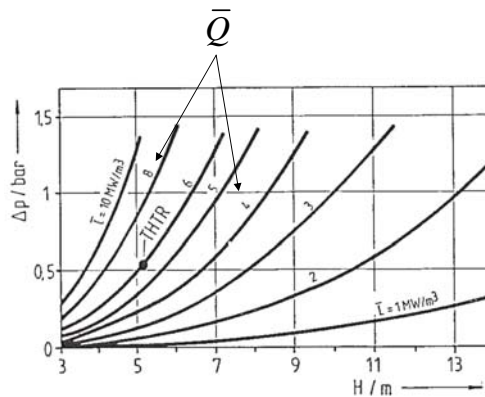
Duderstadt and Hamilton, Nuclear Reactor Analysis, 1976

# Maximum reactor core height

Pressure drop:  $\Delta p \sim \frac{\bar{Q}^2 H^3}{\rho \Delta T^2}$

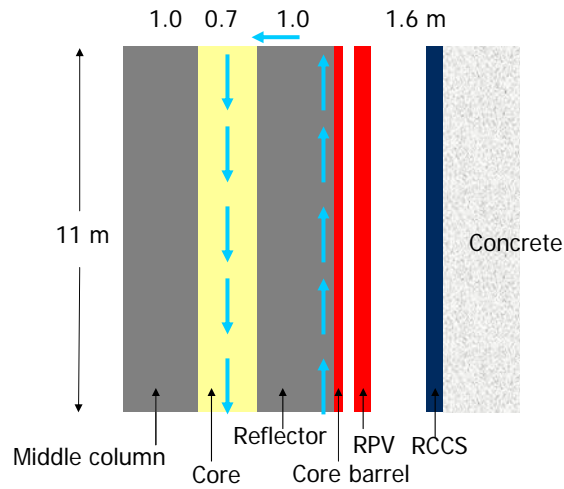
Pumping power:  $P_p = \frac{\Delta p}{\rho} \dot{m}$

(In practice  $\Delta p < 0.02 p$ )

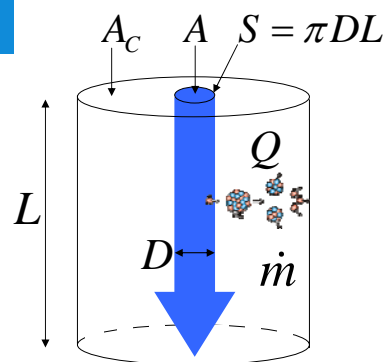


Kugeler and Schulten, Hochtemperatur Reaktortechnik, 1989

## Reactor core layout



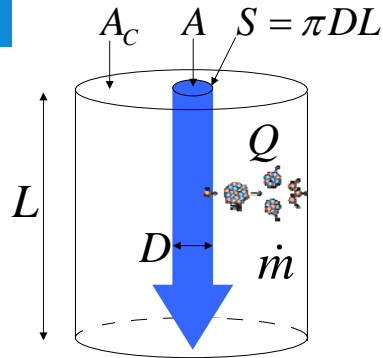
## Gas coolant choice



Mass flow	$\dot{m} = \rho VA$
Power	$Q = \dot{m} C_p (T_{out} - T_{in})$ $= h S \Delta t$
Pressure drop	$\Delta p = \frac{1}{2} \rho V^2 \left( \frac{4fL}{D} \right)$
Pumping power	$P_p = \frac{\Delta p}{\rho} \dot{m}$
Gas law	$P = \frac{\rho RT}{M}$

Melese and Katz, Thermal and Flow Design of Helium-cooled Reactors, ANS, 1984

## Gas coolant choice



$$\frac{Q}{A_c} \propto \sqrt{\frac{c_p^3}{M}}$$

$$\left( \begin{array}{l} c_p = \text{molar heat capacity} \\ M = \text{molar mass} \end{array} \right)$$

Melese and Katz, Thermal and Flow Design of Helium-cooled Reactors, ANS, 1984

## Gas coolant choice

Table 15. Internal energy  $U$  and specific heat capacities  $C$  of gases

Gas	Monatomic	Diatomic	Polyatomic
$f_{tr}$	3	3	3
$f_{rot}$	0	2	3
$f_{vib}$	0	assumed 0	assumed 0
Total	3	5	6
$u \text{ mol}^{-1}$	$\frac{3}{2}kT$	$\frac{5}{2}kT$	$\frac{6}{2}kT$
$U \text{ mol}^{-1}$	$\frac{3}{2}RT$	$\frac{5}{2}RT$	$\frac{6}{2}RT$
$C_v = \left(\frac{\partial U}{\partial T}\right)_v$	$\frac{3}{2}R$	$\frac{5}{2}R$	$3R$
$C_p = C_v + R$	$\frac{5}{2}R$	$\frac{7}{2}R$	$4R$
$\gamma = \frac{C_p}{C_v}$	$\frac{5}{3}$	$\frac{7}{5}$	$\frac{4}{3}$
$C_v$ in units of $R/2 \text{ mol}^{-1}$ :			
Theoretical	3	5	6
Observed	Ar: 3 He: 3	H <sub>2</sub> : 4.9 O <sub>2</sub> : 5.0 N <sub>2</sub> : 4.6 Cl <sub>2</sub> : 6	H <sub>2</sub> S: 6 CS <sub>2</sub> : 10

Tabor, Gases Liquids and Solids, 1979

## Gas coolant choice

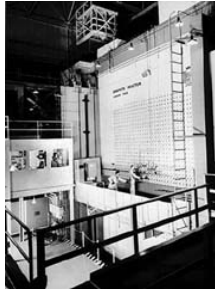
Gas	Power for fixed frontal area ( $Q/A_c$ )	Heat transfer area for fixed flow area	Pressure for a given system pressure
Helium	1.00	1.00	1.00
CO <sub>2</sub>	1.22	1.32	2.52
H <sub>2</sub>	2.41	1.09	1.42
Steam	1.18	1.60	1.96
Air	0.70	1.24	1.53

Melese and Katz, Thermal and Flow Design of Helium-cooled Reactors, ANS, 1984

## History of gas-cooled reactors

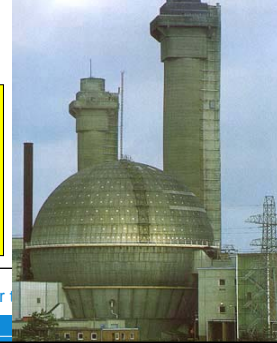
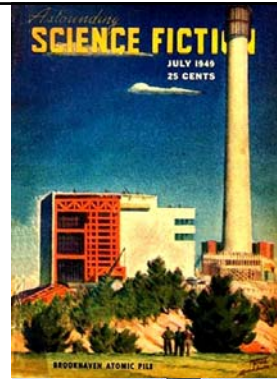


## Early Gas-Cooled Reactors



X-10 reactor in Oak Ridge, 1943  
3.5 MW, air-cooled

- 2 MW reactor in Saclay, 1951, N<sub>2</sub> cooled (later CO<sub>2</sub>)
- Calder Hall reactors, 1953, CO<sub>2</sub> cooled
- 166 MWe reactor in Tokai, 1966, CO<sub>2</sub> cooled
- Magnox and AGRs in the UK, CO<sub>2</sub> cooled



## History of High Temperature Reactors

Reactor name	Power (th/e) (MW)	T <sub>in</sub> (°C)	T <sub>out</sub> (°C)	Pressure (bar)	Operation period	Power density (MW/m <sup>3</sup> )
Dragon	20 / -	350	750	20	1965-1976	14
AVR	46 / 15	270	950	11	1967-1988	2.5
Peach Bottom	115 / 40	344	725	23	1967-1974	8.3

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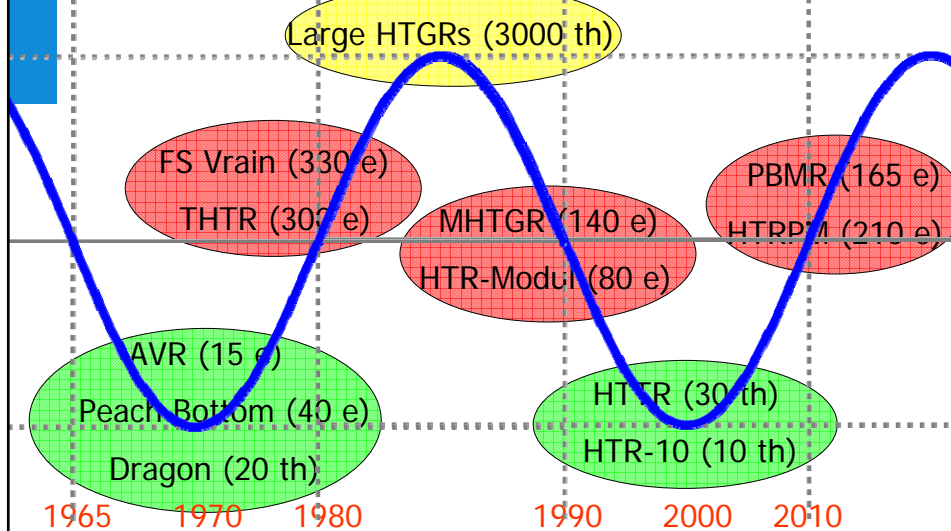
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HTR-Modul	200 / 80	250	750	66		3.0
MHTGR	350 / 140	320	690	64		5.9

## History of High Temperature Reactors

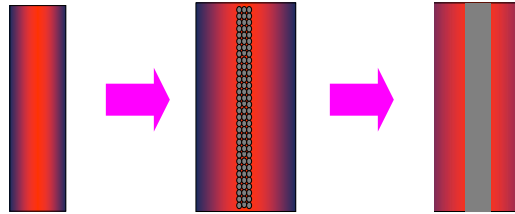
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HTR	30 / -	395	950	40	1998-	2.5
HTR-10	10 / -	250	700	30	2000-	2

## History of High Temperature Reactors



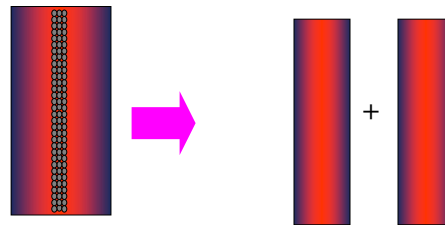
## Current developments

PBMR



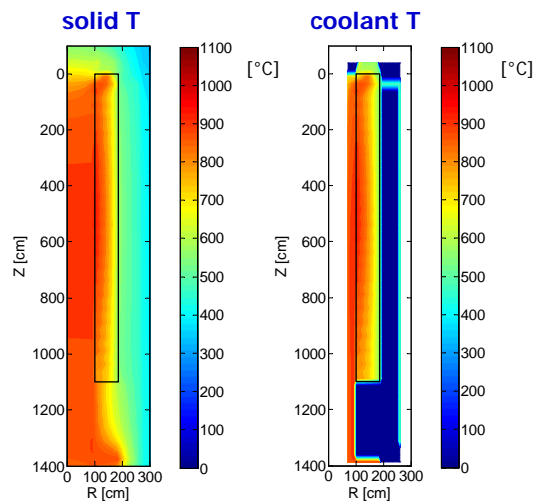
Koster *et al.*, Nucl. Eng. Des. 222(2003) 231

HTR-PM



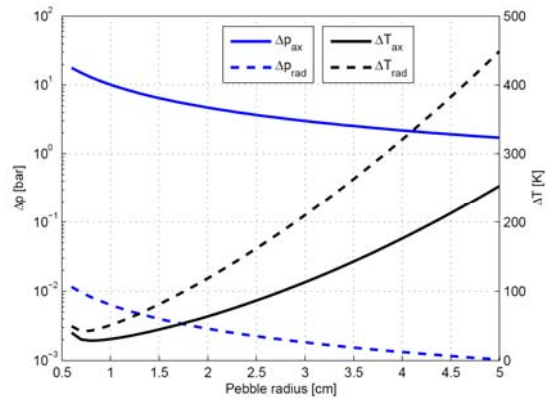
Zhengy and Shi, HTR2008, Washington

## Future developments: Radial cooling



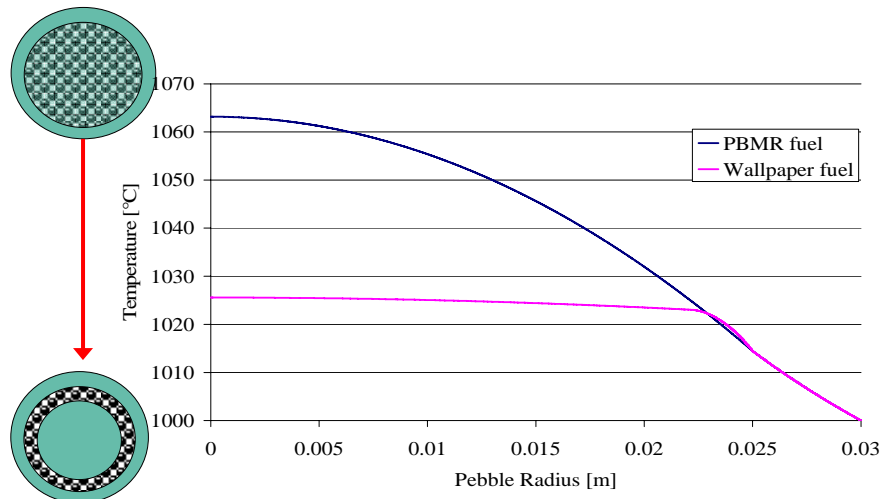
Boer *et al.*, HTR2008, Washington

## Future developments: Radial cooling



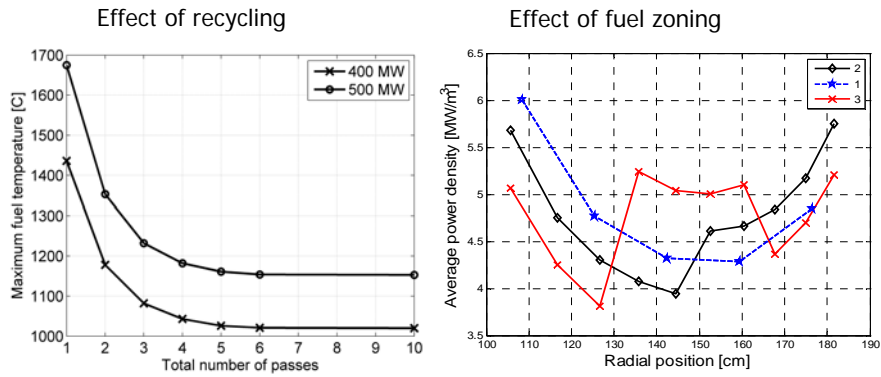
Boer *et al*, HTR2008, Washington

## Future developments: Wall paper fuel



Marmier *et al*, HTR2008, Washington

# Future developments: Optimization



Brian Boer, TU-Delft

# Summary

